# ADVANCED PURIFICATION OF INDUSTRIAL AND MIXED WASTEWATER BY COMBINED MEMBRANE FILTRATION AND SONOCHEMICAL TECHNOLOGIES

Enrico Fatarella<sup>1</sup> Irene Cioni<sup>1</sup> Cecilia Caretti<sup>2</sup> Enrico Venturini degli Esposti<sup>1</sup> Ester Coppini<sup>3</sup> <sup>1</sup>Next Technology Tecnotessile – Prato (Italy) <sup>2</sup>Civil Engeneering Department - University of Florence <sup>3</sup>GIDA Spa – Prato (Italy)

# ABSTRACT

The textile sector plays a critical role in this context, because textile companies are large users of water - typically 0.2-0.5 m3 are needed to produce 1 kg of finished product [1] – and they are historically concentrated in districts (e.g. Prato in Italy) located in Southern Member States, such as Italy, Spain and Portugal, which are facing more and more longer periods of drought and therefore are strongly in the need to preserve the availability of water for potable use. The finishing processes (i.e. pre-treatment, dyeing, printing and special finishing) are especially polluting and resource consuming in terms of water, energy and chemicals. Almost the entire of water used in textile production is discharged and, on average, the effluents volume covers 90-95% of the water used [2].

According to that, a new Ultrafiltration/Sonichemical combined process has been investigated on textile wastewater by evaluating the reduction of the pollution load induced by physical separation and by chemical oxidation promoted by Ultrasound cavitation. The experimental campaign carried out at the Municipal Wastewater treatment Plant in Prato showed that the quality of the treated water reaches the target reported in literature [3] for textile manufacturing sectors. An estimation of the costs of the purified water has been assessed and the combined process seems to be promising for further development.

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# **KEYWORDS**

textile wastewater; mixed wastewater, Ultrafiltration, Ultrasound

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## **1 INTRODUCTION**

Industrial wastewaters contain pollutants recalcitrant to conventional oxidation and biological treatments which must be effectively removed or degraded for water reuse and/or recycle. For this aim the use of advanced oxidation processes (AOPs) is of increasing interest and application. AOPs produce in situ transitory species (mainly hydroxyl radicals) which aid in the degradation process until the target pollutant species are partially or completely converted to more simple compounds. In the recent years, membrane filtration processes have been increasingly applied for the refinement of reclaimed wastewater to be reused because they have the advantages of gaining several positive effects on water quality, saving space and chemicals. Although membrane processes can allow also the separation of low molecular weight and ions to produce permeate colorless and low in total salinity, micro-filtration (MF) and ultra-filtration (UF) are usually used, for refinement of industrial wastewater to be reused, to remove particles, colloids and macromolecules. In the case of reclaimed textile wastewater MF and UF permeate is very low in turbidity and suspended solids, but due to its residual color it cannot be directly reused for some wet textile processes such as dyeing. The combined treatment of membrane filtration and ultrasound treatment seems to be a viable alternative for the refinement of treated effluent to be reused. Within the PURIFAST project, this novel approach, which has not yet been employed on the full industrial scale, will be experienced at pilot scale, in different contexts. In the first part of the pilot plant tests, the combined treatment has been experienced at the Baciacavallo WWTP (managed by GIDA SpA) for the refinement of the reclaimed effluent to be reused in wet textile processes. The combination of ultrafiltration and the ultrasound treatment has been compared to alternative tertiary treatments applied by GIDA SpA. At Baciacavallo WWTP (about 750,000 p.e., maximum flow capacity of 6,000 m<sup>3</sup>/h) almost 70% of incoming wastewater originates in the textile industry and is characterized by high concentrations of surfactants and dyes. Before to be discharged, the secondary effluent is refined using a coagulation-flocculation treatment and ozonation. A share of the reclaimed wastewater (up to 4 Mm<sup>3</sup>y<sup>-1</sup>) undergoes further refinement and is reused for wet textile processes (see figure 1 for a layout of the system). At present reclaimed wastewater is refined with the following treatment train: coagulationflocculation, low pressure sand filtration and ozonation.

# **2 MATERIAL AND METHODS**

The effluents of the WWTP at Baciacavallo have been fed into the small scale prototypes according to the configuration that will be described and detailed in the section "Testing design configuration". Two different pilots (a UF pilot provided by Inge and a US device provided by LAVO) have been used for the realisation of the Pilot Scale Tests. A summary of the main characteristics of the realised pilots is reported in the tables below.

UF Pilot (INGE)	
Parameter	Description
Membrane configuration	Capillaries working in dead-end configuration (inside/outside)
Number of membrane	1 membranes: UF100
Pore size of the membrane	0.02 μm
Capillary diameter	1.5 mm (UF100)
Membrane area	$0.2 \text{ m}^2$ for each membrane
Feed Flow	10 l/h for each membrane
Raw water flux	$50 \ l/m^2h$
Pre-filter pore size	300 μm

Ultrasonic equipment (LAVO)

Parameter	Description
Frequency	350 kHz
Transducer geometry	Cup horn
Number of transducer	24 arranged in three independent groups
Power per US group	1.5 W/l (1 group working)
	3.1 W/l (2 groups working)
	4.7 W/l (3 groups working)
Acoustic power	72.5
Radical formation rate	5.52 μmol/l min

The two pilots have been installed according to the following configuration.

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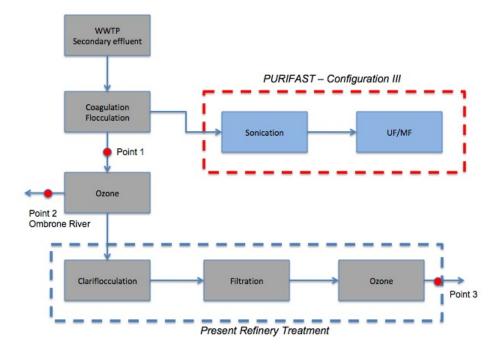


Figure 1 - Configuration tested within PURIFAST project (in blue) compared with the conventional treatment used at GIDA (in grey). The conventional refinery treatment applied at GIDA has been highlighted.

The characterisation of the filtration system has been done by continuously monitoring the following parameters: Transmembrane Pressure (TMP); Permeability (Lp) and Fluxes (F). In fact, TMP is defined as the difference in pressure between the raw water side (retentate) of the membrane and the filtrated water side (permeate) of the membrane. The pressure is the driving force for the membrane filtration. Since we are working at constant flow, an increase in the transmembrane means that a deposit cake is present on the surface of the membrane. The hydraulic permeability (Lp) is a parameter that reflects the relationship between the Flux and the TMP. A decrease in the permeability means that some fouling on the membrane is occurring. In order to define the best filtration conditions (production time, backwashes frequency, chemical cleaning frequencies) during the experimental campaigns, sustainable operating conditions have been researched. Sustainable operating conditions mean that for a fixed flux, the TMP increase is not too fast and can be stabilized over the time thanks to frequent hydraulic backwash and chemical cleans.

Chemical and physical characterisation of the effluent has been done by investigating the parameters selected for textile reuse on a daily basis (table 1).

Parameter	Unit	Standard Tests
pН	-	pH meter
Conductivity	µS/cm	Conductimeter
Turbidity	NTU	IRSA 2120
Total Suspended Solids (TSS)	mg/L	IRSA 2050
Hardness	mg/L	Merk, Dr. Lange – Tritation with EDTA
Colour	A/nm	UV/Vis spectrophotometer range 400-700 nm
Silica (SiO <sub>2</sub> )	mg/L	Dr. Lange - DIN 38405-D21
Chlorides	mg/L	Dr. Lange
Sulphates	mg/L	Merk, Dr. Lange - EPA 375.4 – BaCl <sub>2</sub> method
Chemical Oxygen Demand (COD)	mg/L (O <sub>2</sub> )	Dr. Lange, Merk - DIN38409 - ISO6060
Total Organic Carbon (TOC)	mg/L (CO <sub>2</sub> )	Dr. Lange - DIN30409 H3
Biochemical Oxygen Demand (BOD <sub>5</sub> )	mg/L (O <sub>2</sub> )	Respirometric analysis
Total Surfactants (TS)	mg/L	Computed as MBAS + BiAS
Toxicity	% immobilization	Daphnia Magna - DAPHTOX kit F
Silt Density Index (SDI)	-	

The Silt Density Index has been measured by filtering the effluent coming from the UF or the combined process by using a Millipore filter (pore size 0.45 nm). The duration of the trial is 15 minutes and according to this condition the SDI have been computed according to the following equation:

$$SDI = \frac{100(1 - (t_i/t_f))}{t}$$

where  $t_i$  = time required to filter 500 ml and  $t_f$  =  $t_i$  + time required to filter additional 500 ml.

## **3 RESULTS AND DISCUSSION**

In the table below (table 2) a summary of the concerning the quality of the wastewater inlet to the pilot and coming from the ozonation processes (these data will be compared with the performances of the Ultrasonic treatment) during the experimental campaign.

Table 2 – Quality of the effluent coming from point 1 and point 2 at Baciacavallo WWTP

Parameter	Unit	Before ozonation	After ozonation	PURIFAST Target	
		Average	Average		
pН	-	7.4	7.3	6-8	
Conductivity	µS/cm	1686	1657	≤ <b>3</b> 000	
Turbidity	NTU	5.5	6.8	≤ 5	
TSS	mg/L	10.7	14.5	≤ 5	
Hardness	mg/L	N.A.	N.A.	≤ 50	
Colour	A/nm	16.38	8.21	≤ 2	
SiO <sub>2</sub>	mg/L	6.34	6.9	≤ 25	
Chlorides	mg/L	460	461	≤ 500	
Sulphates	mg/L	169	155	≤ <b>3</b> 00	
COD	mg/L (O <sub>2</sub> )	47.4	46	≤ 35	
TS	mg/L	0.39	0.29	≤ 0.5	
Toxicity	% immobilization	Non toxic	Non toxic	Non toxic	
SDI		N.A.	N.A.	5	

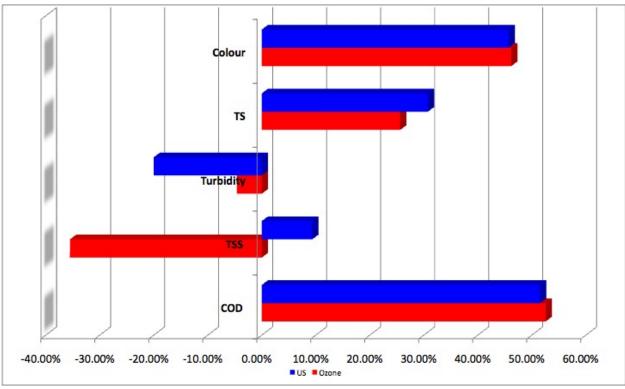
## 3.1 Test with Ultrasonic equipment provided by LAVO

In order to reduce the impact of the fouling induced by the high pollution load of the non ozonised wastewater a new configuration have been tested: the performances of the conventional AOP process performed at GIDA (ozone treatment with a dosing of ozone = 19 g/m<sup>3</sup>) have been compared with the one achieved by treating the effluent from the clariflocculation with the Ultrasonic treatment. The following results have been obtained (table 3).

	Unit	Ozonation	US (non ozonated water)			PURIFAST
Parameter			Low value	Max Value	Average	Target
pН	-	7.37	7.1	7.5	7.1	6-8
Conductivity	μS/cm	1657	1590	2380	1847	≤ 3000
Turbidity	NTU	6.8	3.6	10.0	7.8	≤ 5
TSS	mg/L	14.5	6.8	12.8	9.7	≤ 5
Hardness	mg/L	32.6	29.8	31.8	30.2	≤ 50
Colour	A/nm	8.21	4.45	10.78	8.89	$\leq 2$
SiO <sub>2</sub>	mg/L	6.9	6.07	9.55	9.06	≤ 25
Chlorides	mg/L	461	322.2	390.9	340.5	≤ 500
Sulphates	mg/L	155	133	244	201	≤ 300
COD	mg/L (O <sub>2</sub> )	46.0	32.0	50.1	47.2	≤ 35
TS	mg/L	0.29	0.14	0.32	0.27	≤ 0.5
Toxicity	% immobiliza tion	Non toxic	Non toxic	Non toxic	Non toxic	Non toxic
SDI		-	-	-	-	5

# Table 3 - Results of the chemical and physical characterisation of treated wastewater with US

The effectiveness of the Ultrasonic treatment in the removal (%) of the most critical parameters has been evaluated (Figure 2).



*Figure 2 – Comparison of the performance of primary ozonation and Ultrasonic treatment* 

The data collected in the figure showed that almost the same performances can be ensured by the US in comparison with ozone. According to that, the US seems to be a promising alternative to the primary ozonation.

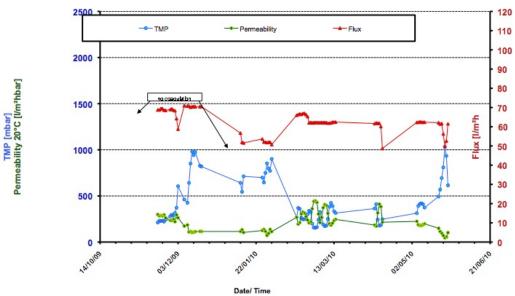
# 3.2 Test with UF pilot provided by INGE

The optimal process conditions for the Ultrafiltration membrane UF100 are listed in table 4.

Working parameter	Value
Flux	60 l/hm <sup>2</sup>
Production time	15 min
Backwash time	40 sec
Backwash flow	60 l/h (filtrate water)
Chemical Enhanced Backwash (CEB)	1 every 4 production cycles by using:
	30 min. 1 g/l NaOH
	15 min. 2 g/l H <sub>2</sub> SO <sub>4</sub>
Coagulation dose	6 mg/L polyaluminiumhydroxidchlorisulfat
Membrane Cleaning in Place (CIP)	none

*Table 4 - Inge pilot plant operating conditions for UF100* 

In fact, by applying these conditions a quite constant behaviour in the flux of the filtration systems can be ensured over a period of 6 months, as shown in the figure 3.



#### Purifast UF100; 20.11.2009 - 25.05.2010

Figure 3 – Hydraulic performances of UF100 system

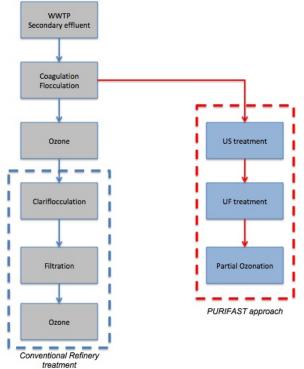
The tests showed that the following hydraulic performances at a constant value of flux (50 L/m2h) can be ensured in this configuration: TMP (average value): 265 mbar Lp (average value): 245 l/nm<sup>2</sup>bar

By applying this conditions to the effluent coming from the US treatment the following parameters have been achieved (Table5).

	Unit	US (non ozon	PURIFAST		
Parameter		Low value	Max Value	Average	Target
pН	-	7.0	7.3	7.1*	6-8
Conductivity	μS/cm	1489	2260	1847	≤ <b>3000</b>
Turbidity	NTU	0.5	0.8	0.66	$\leq 5$
TSS	mg/L	-	-	≤ 5	≤ <b>5</b>
Hardness	mg/L	33.6	43.2	37.1	$\leq 50$
Colour	A/nm	0.29	0.80	0.56	$\leq 2$
SiO <sub>2</sub>	mg/L	6.78	9.10	7.45	≤ 25
Chlorides	mg/L	288.0	307.00	304.2	$\leq 500$
Sulphates	mg/L	134	228	210.6	≤ <b>3</b> 00
COD	mg/L (O <sub>2</sub> )	31.0	49.0	37.6	≤ <b>3</b> 5
TS	mg/L	0.12	0.33	0.21	$\leq 0.5$
Toxicity	% immobilization	Non toxic	Non toxic	Non toxic	Non toxic
SDI		-	-	4 - 6	5

*Table 5 - Results of the chemical and physical characterisation of treated wastewater with the combined process* 

With the exception of the colour, the UF system is able to significantly reduce the solid charge of the effluent. In order to overcome this problem two approach can be investigated; a more suitable dosing of hydrogen peroxide (its overdosing seems to be responsible for this data) can be made or a new design of the purification treatment layout has to be done. According to the project results the following treatment steps can be proposed.



*Figure 4 - Layout of the PURIFAST approch at GIDA compared with the conventional one* 

# 4 CONCLUSIONS

The activities carried out within the PURIFAST project seem to confirm that the combination of Ultrasonic treatment and Ultrafiltration is a promising approach for the purification of textile and mixed wastewater. In fact, the cavitation phenomena related with the bubble collapses in the US equipment is able to generated hydroxyl radical and to catalyse the dissociation of hydrogen peroxide enabling to degrade organic pollutants dissolved in the effluents. Furthermore, the usage of a user-friendly technology such as Ultrasound should represent a benefit according to the low investment costs required for the purchasing of the apparatus and to the lower usage of toxic compounds (ozone is an high toxic gas and the usage of inappropriate amount of ozone for wastewater treatment can generate toxic intermediates as reported in literature [4]).

Moreover, the combination of an AOP with UF system allow to reduce the amount of solid particles and pollutants responsible for a significant amount of the COD load. The problem related with the overdosing of hydrogen peroxide could be easily solved by implementing a dosing systems or by using a partial ozonation.

A preliminary economical evaluation for the proposed approach has been done: a overall cost of around  $1.39 \notin m^3$  for the Combination US and INGE UF system with sonochemical treatment carried out for 4 h is expected. This is quite high but it is promising according to the cost of fresh water in Europe (in countries such as Sweden, Germany is around  $2 \notin m^3$ ) considering that a reduction up to 70% is expected at full scale.

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